

high accuracy is required, the sample can be taken to dryness on a hot plate and the residue dissolved in the appropriate volume of water to bring it into the optimum range of the calibration curve.

11.4.2 Container No. 3 (Silica Gel). This step may be conducted in the field. Weigh the spent silica gel (or silica gel plus impinger) to the nearest 0.5 g; record this weight.

11.5 Check for Matrix Effects. Use the Method of Standard Additions as follows to check at least one sample from each source for matrix effects on the Pb results:

11.5.1 Add or spike an equal volume of standard solution to an aliquot of the sample solution.

11.5.2 Measure the absorbance of the resulting solution and the absorbance of an aliquot of unspiked sample.

11.5.3 Calculate the Pb concentration  $C_m$  in  $\mu\text{g/ml}$  of the sample solution using Equation 12-1 in Section 12.5.

Volume corrections will not be required if the solutions as analyzed have been made to the same final volume. Therefore,  $C_m$  and  $C_a$  represent Pb concentration before dilutions.

Method of Standard Additions procedures described on pages 9-4 and 9-5 of the section entitled "General Information" of the Perkin Elmer Corporation Atomic Absorption Spectrophotometry Manual, Number 303-0152 (Reference 1 in Section 17.0) may also be used. In any event, if the results of the Method of Standard Additions procedure used on the single source sample do not agree to within  $\pm 5$  percent of the value obtained by the routine atomic absorption analysis, then reanalyze all samples from the source using the Method of Standard Additions procedure.

## 12.0 Data Analysis and Calculations

### 12.1 Nomenclature.

$A_m$  = Absorbance of the sample solution.

$A_n$  = Cross-sectional area of nozzle,  $\text{m}^2$  ( $\text{ft}^2$ ).

$A_i$  = Absorbance of the spiked sample solution.

$B_{ws}$  = Water in the gas stream, proportion by volume.

$C_a$  = Lead concentration in standard solution,  $\mu\text{g/ml}$ .

$C_m$  = Lead concentration in sample solution analyzed during check for matrix effects,  $\mu\text{g/ml}$ .

$C_s$  = Lead concentration in stack gas, dry basis, converted to standard conditions,  $\text{mg/dscm}$  ( $\text{gr/dscf}$ ).

$I$  = Percent of isokinetic sampling.

$L_i$  = Individual leakage rate observed during the leak-check conducted prior to the first component change,  $\text{m}^3/\text{min}$  ( $\text{ft}^3/\text{min}$ )

$L_a$  = Maximum acceptable leakage rate for either a pretest leak-check or for a leak-check following a component change; equal to  $0.00057 \text{ m}^3/\text{min}$  ( $0.020 \text{ cfm}$ ) or 4

percent of the average sampling rate, whichever is less.

$L_i$  = Individual leakage rate observed during the leak-check conducted prior to the "ith" component change ( $i = 1, 2, 3, \dots, n$ ),  $\text{m}^3/\text{min}$  ( $\text{cfm}$ ).

$L_p$  = Leakage rate observed during the post-test leak-check,  $\text{m}^3/\text{min}$  ( $\text{cfm}$ ).

$m_t$  = Total weight of lead collected in the sample,  $\mu\text{g}$ .

$M_w$  = Molecular weight of water,  $18.0 \text{ g/g-mole}$  ( $18.0 \text{ lb/lb-mole}$ ).

$P_{\text{bar}}$  = Barometric pressure at the sampling site,  $\text{mm Hg}$  ( $\text{in. Hg}$ ).

$P_s$  = Absolute stack gas pressure,  $\text{mm Hg}$  ( $\text{in. Hg}$ ).

$P_{\text{std}}$  = Standard absolute pressure,  $760 \text{ mm Hg}$  ( $29.92 \text{ in. Hg}$ ).

$R$  = Ideal gas constant,  $0.06236 [(\text{mm Hg}) (\text{m}^3)/[^\circ\text{K}) (\text{g-mole})]$   $\{21.85 [(\text{in. Hg}) (\text{ft}^3)/[^\circ\text{R}) (\text{lb-mole})]\}$ .

$T_m$  = Absolute average dry gas meter temperature (see Figure 5-3 of Method 5),  $^\circ\text{K}$  ( $^\circ\text{R}$ ).

$T_{\text{std}}$  = Standard absolute temperature,  $293 \text{ }^\circ\text{K}$  ( $528 \text{ }^\circ\text{R}$ ).

$v_s$  = Stack gas velocity,  $\text{m/sec}$  ( $\text{ft/sec}$ ).

$V_m$  = Volume of gas sample as measured by the dry gas meter, dry basis,  $\text{m}^3$  ( $\text{ft}^3$ ).

$V_{m(\text{std})}$  = Volume of gas sample as measured by the dry gas meter, corrected to standard conditions,  $\text{m}^3$  ( $\text{ft}^3$ ).

$V_{w(\text{std})}$  = Volume of water vapor collected in the sampling train, corrected to standard conditions,  $\text{m}^3$  ( $\text{ft}^3$ ).

$Y$  = Dry gas meter calibration factor.

$\Delta H$  = Average pressure differential across the orifice meter (see Figure 5-3 of Method 5),  $\text{mm H}_2\text{O}$  ( $\text{in. H}_2\text{O}$ ).

$\theta$  = Total sampling time,  $\text{min}$ .

$\theta_i$  = Sampling time interval, from the beginning of a run until the first component change,  $\text{min}$ .

$\theta_i$  = Sampling time interval, between two successive component changes, beginning with the interval between the first and second changes,  $\text{min}$ .

$\theta_p$  = Sampling time interval, from the final ( $n^{\text{th}}$ ) component change until the end of the sampling run,  $\text{min}$ .

$\rho_w$  = Density of water,  $0.9982 \text{ g/ml}$  ( $0.002201 \text{ lb/ml}$ ).

12.2 Average Dry Gas Meter Temperatures ( $T_m$ ) and Average Orifice Pressure Drop ( $\Delta H$ ). See data sheet (Figure 5-3 of Method 5).

12.3 Dry Gas Volume, Volume of Water Vapor, and Moisture Content. Using data obtained in this test, calculate  $V_{m(\text{std})}$ ,  $V_{w(\text{std})}$ , and  $B_{ws}$  according to the procedures outlined in Method 5, Sections 12.3 through 12.5.

12.4 Total Lead in Source Sample. For each source sample, correct the average absorbance for the contribution of the filter blank and the  $0.1 \text{ N HNO}_3$  blank. Use the calibration curve and this corrected absorbance to determine the Pb concentration in the